

## Elastic energy - gradient expansion

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Energy of a deformed body can not depend on displacement itself because for uniform displacement energy is not changed.

Thus it can depend only on gradients of displacement  $\frac{\partial u_i}{\partial x_k}$

One such term in the elastic energy would be

$$\lambda \left( \frac{\partial u_i}{\partial x_i} \right)^2 = \lambda (\text{div } \vec{u})^2$$

Another one

$$\sum_{i,k} \left( \frac{\partial u_i}{\partial x_k} \right)^2$$

However arbitrary gradients are not allowed because the energy is also invariant with respect to uniform rotations

For rotation on an infinitesimal angle  $\delta \Omega$

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$$\vec{u} = \delta \vec{\Omega} \times \vec{r}$$

$$\text{Thus } \delta \vec{\Omega} = \frac{\text{rot } \vec{u}}{3}$$

Since energy should not depend on  $\delta \Omega$   
it should not contain  $[\text{rot } u]^2 \Rightarrow$  from

• the gradient term  $\left(\frac{\partial u_i}{\partial x_k}\right)^2$  we should  
exclude antisymmetric part  $\frac{\partial u_i}{\partial x_k} - \frac{\partial u_k}{\partial x_i}$

As a result we arrive to

elastic energy

$$\bullet F = \int dV \left[ \frac{\lambda}{2} (\text{div } \vec{u})^2 + \mu (u_{ik})^2 \right]$$

$$\text{with } u_{ik} = \frac{1}{2} \left( \frac{\partial u_i}{\partial x_k} + \frac{\partial u_k}{\partial x_i} \right)$$

## Thermal expansion

Let us consider deformations due to change in the temperature of the body.

At  $T = T_0$  body is assumed to be undeformed. If  $T \neq T_0$  the body will be deformed even in the absence of external forces.

• Thus the free energy will contain also linear terms in  $u_{ik}$ .

The only invariant one can make from  $u_{ik}$  is  $u_{ii} = \text{div } \vec{u}$

• Thus

$$F(T) = F_0(T) - KA(T)u_{ii} + \frac{K}{2}u_{ee}^2 + \mu\left(u_{ik} - \frac{1}{3}\delta_{ik}u_{ee}\right)^2$$

If  $T$  is close to  $T_0$  then we can expand  $A(T) = \alpha(T - T_0) + \beta(T - T_0)^2 + \dots$

Keeping only linear term we obtain

$$F(T) = F_0T - K\alpha(T - T_0)u_{ii} + \frac{K}{2}u_{ee}^2 + \mu\left(u_{ik} - \frac{1}{3}\delta_{ik}u_{ee}\right)^2$$

Using  $\delta_{ik} = \frac{\partial F}{\partial u_{ik}}$  we obtain

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$$\delta_{ik} = -K \alpha (T - T_0) \delta_{ik} + K u_{ee} \delta_{ik} + 2\mu \left( u_{ik} - \frac{1}{3} \delta_{ik} u_{ee} \right)$$

In the absence of external forces there can be no internal stresses  $\Rightarrow \delta_{ik} = 0 \Rightarrow$

$$u_{ik} \propto \delta_{ik} \quad \text{and} \quad u_{ee} = \alpha (T - T_0) \Rightarrow$$

- $\frac{\delta V}{V} = \alpha (T - T_0) \Rightarrow \alpha$  - thermal expansion coefficient.

If the body is non-uniformly heated

in the equation of motion  $\frac{\partial \delta_{ik}}{\partial x_k} = 0$

- we should include the term  $-K \alpha (T - T_0) \delta_{ik}$  in  $\delta_{ik}$ . As a result equation from p. 15 reads

$$\frac{3(1-\beta)}{1+\beta} \text{grad div } u - \frac{3(1-2\beta)}{2(1+\beta)} \text{rot rot } u = \alpha \nabla T$$

# Elasticity of crystals

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In general

$$F = \frac{1}{2} \lambda_{iklm} u_{ik} u_{lm}, \quad \delta_{ik} = \lambda_{iklm} u_{lm}$$

elastic modulus tensor

Since  $u_{ik} = u_{ki} \Rightarrow$

- $\lambda_{iklm} = \lambda_{kilm} = \lambda_{ikml} = \lambda_{lmik}$

For the isotropic body we should construct

$\lambda_{iklm}$  out of  $\delta_{jn}$

The only two tensors satisfying symmetry relations are  $\delta_{ik} \delta_{lm}$  and  $\delta_{ie} \delta_{km} + \delta_{im} \delta_{ke}$

- Thus  $\lambda_{iklm} = \lambda \delta_{ik} \delta_{lm} + \mu (\delta_{ie} \delta_{km} + \delta_{im} \delta_{ke})$

and  $F_{el} = \frac{1}{2} \int dV [\lambda u_{ee}^2 + 2\mu u_{ik} u_{ik}]$

In general there are 21 independent components<sup>(21)</sup> of  $\Delta_{iklm}$ . To see it, note, that there are only six independent combinations of  $i, k$  and  $l, m$ . These are denoted by

$$1 = xx, 2 = yy, 3 = zz, 4 = yz, 5 = xz, 6 = xy$$

Then we can use  $C_{\alpha\beta}$  instead of  $\Delta_{iklm}$  with  $\alpha, \beta = 1, 2, \dots, 6$

For  $\alpha = 1$   $\beta$  can be any of 6 numbers

But since  $C_{\alpha\beta} = C_{\beta\alpha}$  then  $C_{12} = C_{21}$  and

for  $\alpha = 2$   $\beta$  is 2, 3, ..., 6 (5 number)

• for  $\alpha = 3$   $\beta$  is 3, 4, 5, 6 etc.

As a result we have

$$6 + 5 + 4 + 3 + 2 + 1 = 21 \text{ independent components}$$

Depending on crystal symmetry, number of components can be reduced.

Tetragonal system

$\lambda_{iklm}$  transforms as  $X_i X_k X_l X_m$

Because of reflection symmetry

•  $x \rightarrow -x, y \rightarrow y, z \rightarrow z$  and

$x \rightarrow x, y \rightarrow -y, z \rightarrow z$

all components with an odd number of like indices vanish.

Further more, a  $90^\circ$  rotation leads to

•  $x \rightarrow y, y \rightarrow -x, z = z \Rightarrow$

$\lambda_{xxxx} = \lambda_{yyyy}, \lambda_{xxzz} = \lambda_{yyzz}, \lambda_{xzzz} = \lambda_{yzzz}$

As a result there are 6 elastic constants

$$F = \frac{1}{2} \lambda_{xxxx} (u_{xx}^2 + u_{yy}^2) + \frac{1}{2} \lambda_{zzzz} u_{zz}^2 +$$
  
$$+ \lambda_{xxzz} (u_{xx} u_{zz} + u_{yy} u_{zz}) + \lambda_{xxyy} u_{xx} u_{yy} +$$
  
$$+ 2 \lambda_{xyxy} u_{xy}^2 + 2 \lambda_{xzzz} (u_{xz}^2 + u_{yz}^2)$$

For the Cubic system

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$x, y$  and  $z$  are equivalent  $\Rightarrow$

$$\lambda_{xxxx} = \lambda_{zzzz}, \quad \lambda_{xxzz} = \lambda_{xyyy}$$

$$\lambda_{xyxy} = \lambda_{xzxz}$$

and one has 3 independent elastic constants.

$$F = \frac{1}{2} \lambda_{xxxx} (u_{xx}^2 + u_{yy}^2 + u_{zz}^2) +$$

$$+ \lambda_{xyxy} (u_{xx}u_{yy} + u_{xx}u_{zz} + u_{yy}u_{zz}) +$$

$$+ 2 \lambda_{xyxz} (u_{xy}^2 + u_{xz}^2 + u_{yz}^2)$$

In general the number of modulus is

Triclinic	21
Monoclinic $C_2, C_s, C_m$	13
Orthorhombic $D_2, C_{2v}, C_{2h}$	9
Tetragonal $C_4, S_4, C_{4h}, C_{4v}, D_{2d}, D_{4h}, D_{4d}$	6
Hexagonal	5
Cubic	3

# Thermal expansion of crystals

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$$u_{ik} = \frac{1}{3} \alpha_{ik} (T - T_0)$$

$\alpha_{ik}$  is symmetric tensor

It has 3 components for

triclinic, monoclinic and orthorhombic,

- 2 components for tetragonal and hexagonal
- and 1 component for cubic lattice.