

Mechanics Fall 2009, Solutions 8

1. Blasting of an industrial chimney

Since the chimney is rotating around 0 we get the equation of motion

$$I \cdot \ddot{\varphi} = Mg \frac{L}{2} \sin \varphi$$

where

$$I = \frac{ML^2}{3}$$

is the moment of inertia of the chimney. We therefore have an angular acceleration of

$$\ddot{\varphi} = \frac{3g \sin \varphi}{2L}$$

In the frame of the falling chimney an element $dm = \frac{M}{L} dx$ experiences a perpendicular force given by

$$dF = -\frac{M}{L} x \ddot{\varphi} dx + \frac{M}{L} g \sin \varphi dx$$

An element at distance x_0 from 0 experiences a torque due to the rest of the chimney above it. This torque is given by

$$\begin{aligned} D(x_0) &= \frac{M}{L} \ddot{\varphi} \int_{x_0}^L x(x-x_0) dx - \frac{M}{L} g \sin \varphi \int_{x_0}^L (x-x_0) dx \\ &= \frac{M}{L} \left[\ddot{\varphi} \left(\frac{x_0^3}{6} - \frac{L^2}{2} x_0 \right) + g \sin \varphi \left(Lx_0 - \frac{x_0^2}{2} \right) \right] + const \end{aligned}$$

The extremal torque is found by

$$\frac{dD(x_0)}{dx_0} = 0$$

with the solutions $x_0 = L/3$ (maximal torque) and $x_0 = L$ (minimal torque). The maximum torque is therefore found at distance $x_0 = L/3$ from 0. This is where the chimney might possibly break.

2. Moments of Inertia

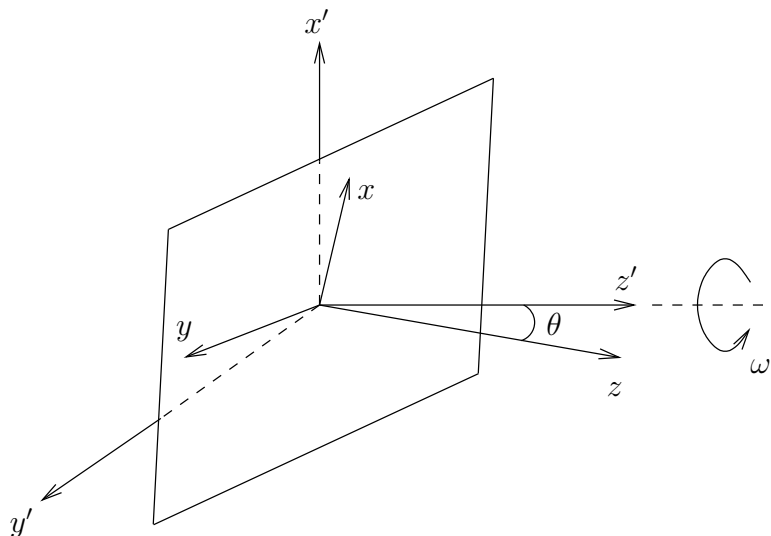


Figure 1: Thin square plate

- (a) Take the origin at the centre O of the square. For a coordinate frame attached to the square, take the plane of the square as the xy -plane with the x - and y -axis parallel to the sides. The z -axis, which is along the normal, makes an angle θ with the z' -axis of the laboratory frame about which the square rotates, as shown in figure 1. We also assume that the x -, z - and z' -axes are coplanar.

Then by symmetry the x -, y - and z -axes are the principal axes of inertia about O , with corresponding moments of inertia

$$I_{xx} = I_{yy} = \frac{ma^2}{12}, \quad I_{zz} = \frac{ma^2}{6},$$

where m is the mass of the square.

- (b) The angular momentum \mathbf{J} resolved along the rotating frame coordinate axes is

$$\begin{pmatrix} J_x \\ J_y \\ J_z \end{pmatrix} = \begin{pmatrix} \frac{ma^2}{12} & 0 & 0 \\ 0 & \frac{ma^2}{12} & 0 \\ 0 & 0 & \frac{ma^2}{6} \end{pmatrix} \begin{pmatrix} \omega \sin \theta \\ 0 \\ \omega \cos \theta \end{pmatrix} = \begin{pmatrix} \frac{ma^2}{12} \omega \sin \theta \\ 0 \\ \frac{ma^2}{6} \omega \sin \theta \end{pmatrix}.$$

We can choose the laboratory frame so that its y' -axis coincides with the y -axis at $t = 0$. Then the unit vectors of the two frames are

related by

$$\begin{aligned}\mathbf{e}_x &= \cos \theta \cos \omega t \mathbf{e}_{x'} + \cos \theta \sin \omega t \mathbf{e}_{y'} + \sin \theta \mathbf{e}_{z'}, \\ \mathbf{e}_y &= -\sin \omega t \mathbf{e}_{x'} + \cos \omega t \mathbf{e}_{y'}, \\ \mathbf{e}_z &= -\sin \theta \cos \omega t \mathbf{e}_{x'} - \sin \theta \sin \omega t \mathbf{e}_{y'} + \cos \theta \mathbf{e}_{z'}.\end{aligned}$$

Hence the angular momentum resolved along the laboratory frame coordinate axes is

$$\begin{aligned}\begin{pmatrix} J_{x'} \\ J_{y'} \\ J_{z'} \end{pmatrix} &= \begin{pmatrix} \cos \theta \cos \omega t & -\sin \omega t & -\sin \theta \cos \omega t \\ \cos \theta \sin \omega t & \cos \omega t & -\sin \theta \sin \omega t \\ \sin \theta & 0 & \cos \theta \end{pmatrix} \begin{pmatrix} \frac{ma^2}{12} \omega \sin \theta \\ 0 \\ \frac{ma^2}{6} \omega \cos \theta \end{pmatrix} \\ &= \begin{pmatrix} -\frac{ma^2}{12} \omega \sin \theta \cos \theta \cos \omega t \\ -\frac{ma^2}{12} \omega \sin \theta \cos \theta \sin \omega t \\ \frac{ma^2}{12} \omega (1 + \cos^2 \theta) \end{pmatrix}.\end{aligned}$$

(c) The torque on the axis in the laboratory frame is given by

$$\mathbf{M} = \frac{d\mathbf{J}}{dt} = \begin{pmatrix} \frac{ma^2}{12} \omega^2 \sin \theta \cos \theta \sin \omega t \\ -\frac{ma^2}{12} \omega^2 \sin \theta \cos \theta \cos \omega t \\ 0 \end{pmatrix}.$$