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Elasticity theory

Elastic energy - gradient expansion

Energy of a deformed body can not depend on displacement itself because for uniform translation energy is not changed. Thus it can depend only on gradient of displacement $\frac{\partial u_i}{\partial x_k}$

For isotropic solid one can construct two

quadratic invariants, from $\frac{\partial u_i}{\partial x_k}$

$$\left(\frac{\partial u_i}{\partial x_i}\right)^2 = (\text{div } \vec{u})^2 \quad \text{and} \quad \sum_{i,k} \left(\frac{\partial u_i}{\partial x_k}\right)^2$$

However, not every gradient of displacement leads to energy change. The energy is also invariant with respect to uniform rotation

Infinitesimal rotation by an angle δR

$$\vec{u} = \delta \vec{R} \times \vec{r} \quad \text{with} \quad \delta \vec{R} = \frac{\text{rot } \vec{u}}{2}$$

Since energy should not depend on $\delta \vec{R}$ thus from the gradient term we should exclude

antisymmetric part and describe deformation

by symmetric tensor $u_{ik} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_k} + \frac{\partial u_k}{\partial x_i} \right)$

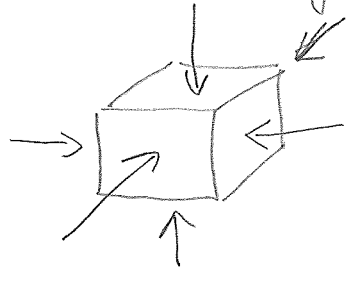
Then elastic energy is

$$F = \frac{\lambda}{2} u_{ii}^2 + \mu u_{ik}^2$$

λ, μ - Lamé coefficients

We can diagonalize u_{ik} at any given point

$$\begin{pmatrix} u_{11} & 0 & 0 \\ 0 & u_{22} & 0 \\ 0 & 0 & u_{33} \end{pmatrix}$$



Then $\vec{u}(x) = \vec{x}' - \vec{x}$, $dx'_i = dx_i + du_i$

$$dx'_1 = (1 + u_{11})dx_1, dx'_2 = (1 + u_{22})dx_2, dx'_3 = (1 + u_{33})dx_3$$

The volume $dV = dx_1 dx_2 dx_3 \Rightarrow$

$$dV' = dV (1 + u_{11})(1 + u_{22})(1 + u_{33}) \approx dV (1 + \sum_i u_{ii})$$

$$dV' = dV (1 + u_{ii}) \quad (\text{we sum over repeating indices})$$

The trace u_{ii} is invariant. Thus the relative volume change is

$$\frac{dV' - dV}{dV} = u_{ii} = \text{div } \vec{u}$$

Stress tensor

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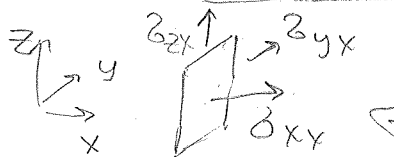
Before the deformation body is in equilibrium. \Rightarrow
After deformation forces arise which tend to return
the body to equilibrium. These forces are called
internal stresses.

It is important that the internal stresses are
due to molecular forces which have very short
range of action. Thus in macroscopic elasticity
theory these forces may be considered as having
zero range of action (we do not consider here
macroscopic electric fields in piezoelectrics).

Consider force acting on some volume Ω . $\int \vec{F} dV$
The total force from the inner part is zero (Newton's
third law). Thus the total force is the force from
the neighbouring parts of the body which can be
considered as applied to the surface \Rightarrow

$$\int \vec{F} dV = \oint \sigma_{ik} dS_k \Rightarrow F_i = \frac{\partial \sigma_{ik}}{\partial x_k}$$

σ_{ik} - stress tensor (symmetric)


 $\left(\sigma_{ik} \text{ is } i\text{-th component of the force acting on the surface } \perp k \right)$

Hydrostatic compression $-p dS_i = -p \delta_{ik} ds_k \Rightarrow$

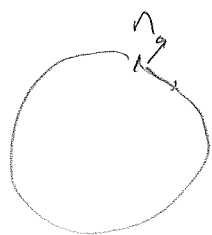
$$\mathcal{Z}_{ik} = -p \delta_{ik}.$$

In equilibrium $\vec{F}_i = 0 \Rightarrow \frac{\partial \mathcal{Z}_{ik}}{\partial x_k} = 0$

If we have external bulk forces (e.g. gravitation) \Rightarrow

$$\frac{\partial \mathcal{Z}_{ik}}{\partial x_k} + \rho g_i = 0 \quad (1)$$

If external forces are applied at the surface \Rightarrow



$$P_i ds = \mathcal{Z}_{ik} ds_k = \mathcal{Z}_{ik} n_k ds \quad (\vec{n} \text{ - normal}) \Rightarrow$$

boundary conditions $\mathcal{Z}_{ik} n_k = P_i$

The work done under deformation

$$\int \delta R dV = \int F_i \delta u_i dV = \int \frac{\partial \mathcal{Z}_{ik}}{\partial x_k} \delta u_i dV =$$

Integrating by parts $= \oint \mathcal{Z}_{ik} \delta u_i ds_k - \int \mathcal{Z}_{ik} \frac{\partial \delta u_i}{\partial x_k} dV$

Taking surface in the first integral to infinity where there are no deformations and using $\mathcal{Z}_{ik} = \mathcal{Z}_{ki}$ we

obtain $\int \delta R dV = - \int \mathcal{Z}_{ik} \delta u_{ik} dV \Rightarrow$

change in the free energy $dF = -SdT - \delta R \Rightarrow$

$$\mathcal{Z}_{ik} = \left(\frac{\partial F}{\partial u_{ik}} \right)_T$$

Hooke's law

(5)

In equilibrium $\sigma_{ik} = 0 = \frac{\partial F}{\partial u_{ik}} \Rightarrow$

Free energy F is quadratic in u_{ik}

From symmetric tensor one can make two quadratic scalars \Rightarrow

$$F = F_0 + \frac{\lambda}{2} u_{ii}^2 + \mu u_{ik}^2$$

λ, μ - Lamé coefficients

If $u_{ii} = 0 \Rightarrow$ volume is unchanged \Rightarrow shear

μ - shear modulus

$$u_{ik} = \underbrace{\left(u_{ik} - \frac{1}{3} \delta_{ik} u_{ee} \right)}_{\text{shear}} + \frac{1}{3} \delta_{ik} \underbrace{u_{ee}}_{\text{compression}}$$

$$F = \mu \left(u_{ik} - \frac{\delta_{ik} u_{ee}}{3} \right)^2 + \frac{\kappa}{2} u_{ee}^2$$

κ - compression modulus, $\kappa = \lambda + \frac{2}{3} \mu$

If $u_{ee} = 0$ then only first term $F = \mu (\dots)^2$

if $u_{ik} \propto \delta_{ik}$ then only the $\frac{\kappa}{2} u_{ee}^2 \Rightarrow$

$$\kappa > 0, \mu > 0$$

$$dF = \left[K U_{ee} \delta_{ik} + 2\mu \left(U_{ik} - \frac{1}{3} \delta_{ik} U_{ee} \right) \right] dU_{ik} \Rightarrow \quad (6)$$

$$\tau_{ik} = K U_{ee} \delta_{ik} + 2\mu \left(U_{ik} - \frac{1}{3} \delta_{ik} U_{ee} \right)$$

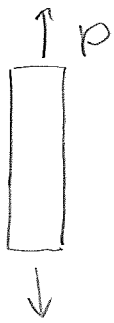
And inverting it we obtain

$$U_{ik} = \frac{1}{9K} \delta_{ik} \tau_{ee} + \frac{1}{2\mu} \left(\tau_{ik} - \frac{1}{3} \delta_{ik} \tau_{ee} \right)$$

Hooke's law

Homogeneous deformations

(strain tensor is constant)



extension

$$\tau_{ik} n_k = P_i \Rightarrow$$

$$\tau_{zz} = P \quad \text{and other components} = 0$$

$$U_{xx} = U_{yy} = -\frac{1}{3} \left(\frac{1}{2\mu} - \frac{1}{3K} \right) P$$

$$U_{zz} = \frac{1}{3} \left(\frac{1}{3K} + \frac{1}{\mu} \right) P = \frac{P}{E}$$

where $E = \frac{9K\mu}{3K + \mu}$ is the coefficient of

extension or the Young's modulus

The ratio of the transverse compression to the longitudinal extension is called the Poisson's ratio

$$u_{xx} = -\beta u_{zz}$$

$$\beta = \frac{1}{2} \frac{3k - 2\mu}{3k + \mu}$$

Since $k, \mu > 0 \Rightarrow -1 < \beta \leq \frac{1}{2}$

In reality, however $0 < \beta \leq \frac{1}{2}$

$$\beta > 0 \Leftrightarrow \lambda > 0.$$

Although not required from thermodynamics

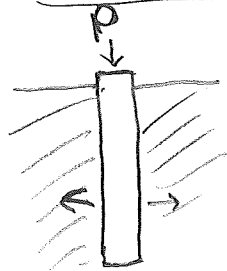
, $\lambda > 0$ is realized in practice

$\beta \rightarrow \frac{1}{2}$ corresponds to the situation, when

$$\mu \ll k$$

Problem 1

Find deformation of a rod whose



sides are fixed in such a way that they cannot move. Find the transverse force it exerts on the medium

In terms of E and β free energy can be rewritten as (8)

$$F = \frac{E}{2(1+\beta)} \left(u_{ik}^2 + \frac{\beta}{1-2\beta} u_{ee}^2 \right)$$

Then $\beta_{ik} = \frac{E}{1+\beta} \left(u_{ik} + \frac{\beta}{1-2\beta} u_{ee} \delta_{ik} \right)$ and

inverting

$$u_{ik} = \frac{1}{E} \left[(1+\beta) \beta_{ik} - \beta \delta_{ik} \beta_{ee} \right]$$

Note, that since F is quadratic in u_{ik} (Hooke's law) it can be rewritten as quadratic in β_{ik} , then one can obtain

$$u_{ik} = \frac{\partial F}{\partial \beta_{ik}}$$

One should emphasize, however, that this equation is consequence of the Hooke's law, whereas $\beta_{ik} = \frac{\partial F}{\partial u_{ik}}$ is general relation of thermodynamics

Equations of equilibrium for isotropic bodies (9)

Let us substitute expression for σ_{ik} in the general expression (1)

$$\frac{\partial \sigma_{ik}}{\partial x_k} + \rho g_i = 0 \Rightarrow$$

$$\frac{E}{2(1+\nu)} \frac{\partial^2 u_i}{\partial x_k^2} + \frac{E}{2(1+\nu)(1-2\nu)} \frac{\partial^2 u_e}{\partial x_i \partial x_e} + \rho g_i = 0$$

Or in vector notations

$$\Delta \vec{u} + \frac{1}{1-2\nu} \text{grad div } \vec{u} = -\rho \vec{g} \frac{2(1+\nu)}{E} \quad (2)$$

Using $\text{rot rot } \vec{u} = \text{grad div } \vec{u} - \Delta \vec{u}$

we can exclude $\Delta \vec{u}$ and obtain

$$\text{grad div } \vec{u} - \frac{1-2\nu}{2(1-\nu)} \text{rot rot } \vec{u} = -\rho \vec{g} \frac{(1+\nu)(1-2\nu)}{E(1-\nu)} \quad (3)$$

function

Some applications

Let us determine deformation of a solid sphere of radius R in its own gravitational field (Earth)

Gravity force in a spherical body is $-g \vec{r}/R$

Substituting it into div \vec{u} equation (3) we obtain

$$\frac{E(1-\beta)}{(1+\beta)(1-2\beta)} \frac{d}{dr} \left(\frac{1}{r^2} \frac{d(r^2 u)}{dr} \right) = 8g \frac{r}{R}$$

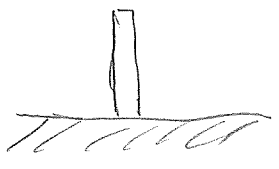
Solution which is finite at $r=0$ and has $\partial_{rr} u = 0$ at $r=R$ is

$$u = - \frac{8gR(1-2\beta)(1+\beta)}{10E(1-\beta)} + \left(\frac{3-\beta}{1+\beta} - \frac{r^2}{R^2} \right)$$

Note, that the substance is compressed ($u_{rr} < 0$) for $r < R \sqrt{(3-\beta)/3(1+\beta)}$ and stretched outside. At the center the pressure is $p = \frac{(3-\beta)gR}{10(1-\beta)}$

Problem 2

Determine the deformation of the long rod standing vertically in a gravitation field



Elasticity of crystals

(11)

In general

$$F = \frac{1}{2} \lambda_{iklm} u_{ik} u_{lm}, \quad \delta_{ik} = \lambda_{iklm} u_{lm}$$

Since $u_{ik} = u_{ki}$ then

$$\lambda_{iklm} = \lambda_{kilm} = \lambda_{ikml} = \lambda_{lmik}$$

As a result of these symmetries in general there are 21 independent components. To see it note that ik can have six independent combinations these are denoted by

$$1 = xx, 2 = yy, 3 = zz, 4 = yz, 5 = xz, 6 = xy$$

Then we can use $C_{\alpha\beta}$ instead of λ_{iklm} with $\alpha, \beta = 1, 2, \dots, 6$.

For $\alpha = 1$ β can be any of 6 numbers.

But since $C_{\alpha\beta} = C_{\beta\alpha}$ then $C_{12} = C_{21}$ and

for $\alpha = 2$ β is 2, 3, ..., 6 (5 numbers)

for $\alpha = 3$ β is 3, 4, 5, 6 etc. As a result

$$6 + 5 + 4 + 3 + 2 + 1 = 21 \text{ independent components}$$

Since orientation is given by the three angles then choosing appropriate frame reduces the number of components to 18.

Example For tetragonal system since

(12)

λ_{iklm} transforms as $X_i X_k X_l X_m$

Then because of symmetry

$$x \rightarrow -x, y \rightarrow y, z \rightarrow z \quad \text{and}$$

$$x \rightarrow x, y \rightarrow -y, z \rightarrow z \quad \text{all components}$$

of λ_{iklm} with an odd number of like suffixes vanish

Further more, a rotation through an angle $\frac{\pi}{2} \rightarrow$

$$x \rightarrow y, y \rightarrow -x, z \rightarrow z \Rightarrow$$

$$\lambda_{xxxx} = \lambda_{yyyy}, \lambda_{xxzz} = \lambda_{yyzz}, \lambda_{xzxz} = \lambda_{yzyz}$$

As a result there are 6 elastic constants

$$F = \frac{1}{2} \lambda_{xxxx} (u_{xx}^2 + u_{yy}^2) + \frac{1}{2} \lambda_{zzzz} u_{zz}^2 + \lambda_{xxzz} (u_{xx} u_{zz} + u_{yy} u_{zz}) \\ + \lambda_{xxyy} u_{xx} u_{yy} + 2\lambda_{xyxy} u_{xy}^2 + 2\lambda_{xzxz} (u_{xz}^2 + u_{yz}^2)$$

Problem 3

Show that for cubic system there are 3 independent elastic constants